

Dynamics and Steering Control of an Autonomous Unicycle

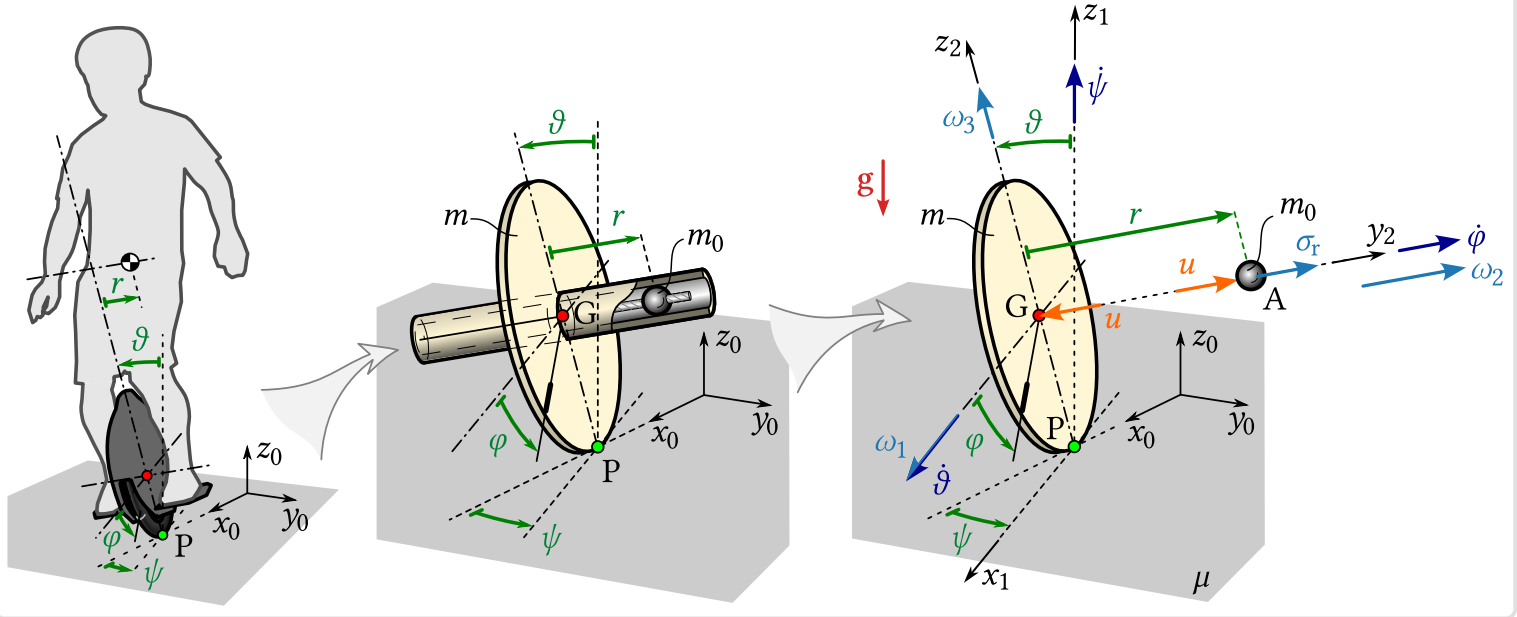
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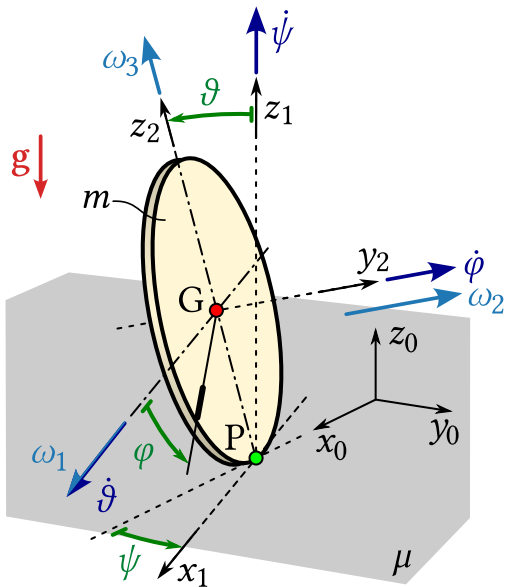


Motivation: unicycles

(Onewheel car)



Mechanical model

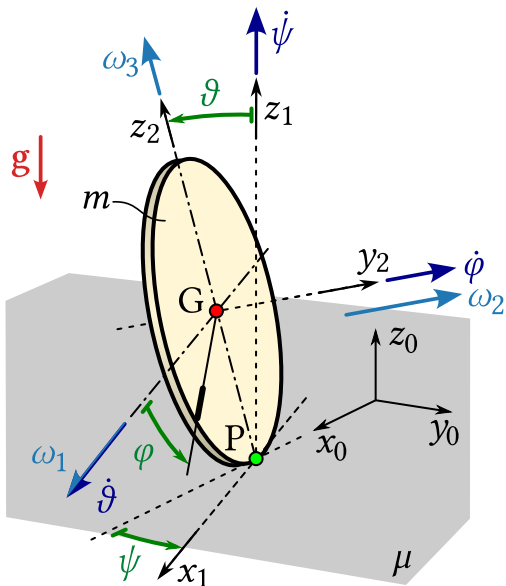


Overview

- ▶ Disc: $m R g$
- ▶ Coordinate frames: $F_0 \xrightarrow{\psi} F_1 \xrightarrow{\vartheta} F_2 \xrightarrow{\varphi} F_3$
- ▶ Natural coordinates: (6 db)
 - $x_G \ y_G \ z_G \ \psi$ (yaw) ϑ (roll tilt) φ (pitch)
- ▶ **Rolling:** constraints
 - ▶ P is the velocity pole: $\mathbf{v}_P = \mathbf{0}$ kinematic

$$\begin{aligned} \dot{x}_G &= \dot{\psi} R \cos \psi \sin \vartheta + \dot{\vartheta} R \sin \psi \cos \vartheta + \dot{\varphi} R \cos \psi \\ \dot{y}_G &= \dot{\psi} R \sin \psi \sin \vartheta - \dot{\vartheta} R \cos \psi \cos \vartheta + \dot{\varphi} R \sin \psi \\ \dot{z}_G &= -R \dot{\vartheta} \sin \vartheta \end{aligned}$$

Mechanical model



Constraints and coordinates

- Constraints: 2 kinematic + 1 geometric

$$\dot{x}_G = \dot{\psi} R \cos \psi \sin \vartheta + \dot{\vartheta} R \sin \psi \cos \vartheta + \dot{\phi} R \cos \psi$$

$$\dot{y}_G = \dot{\psi} R \sin \psi \sin \vartheta - \dot{\vartheta} R \cos \psi \cos \vartheta + \dot{\phi} R \sin \psi$$

$$\dot{z}_G = -R \dot{\vartheta} \sin \vartheta \quad \Rightarrow \quad z_G = R \cos \vartheta$$

- Nonholonomic system → **Appellian approach!**

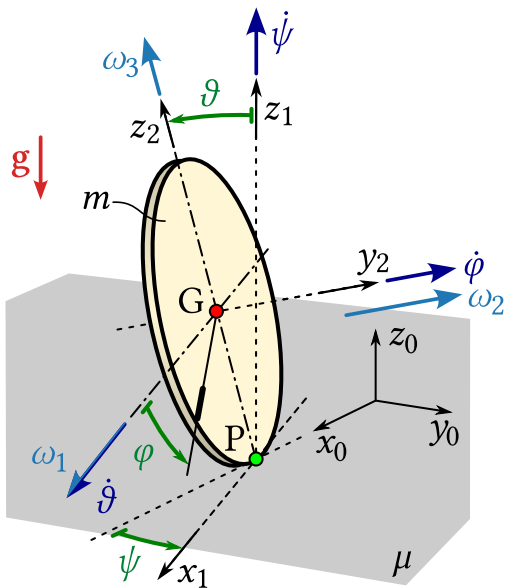
- Generalized coordinates: (5 pcs)

$$x_G \quad y_G \quad \psi (\text{yaw}) \quad \vartheta (\text{tilt}) \quad \phi (\text{pitch})$$

- Pseudo velocities: (3 pcs)

$$\omega_1 := \dot{\vartheta} \quad \omega_2 := \dot{\psi} \sin \vartheta + \dot{\phi} \quad \omega_3 := \dot{\psi} \cos \vartheta$$

Mechanical model



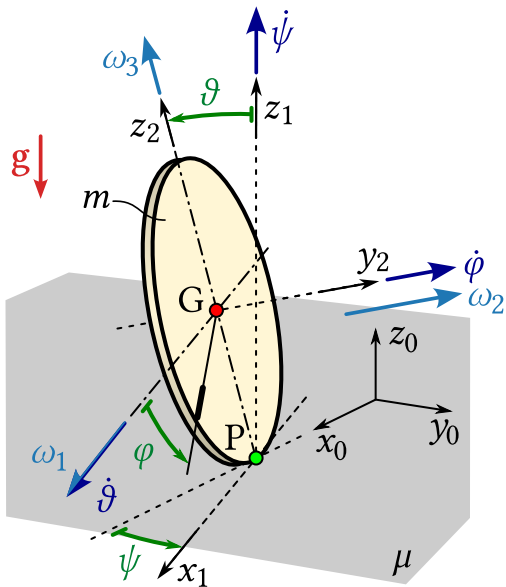
Equations of motion

$$\text{Appell } \frac{\partial S}{\partial \dot{\sigma}_i} = \Pi_i \quad \left\{ \begin{array}{l} \dot{\omega}_1 = \frac{6\omega_2\omega_3}{5} - \frac{\omega_3^2 \tan \vartheta}{5} + \frac{4g \sin \vartheta}{5R} \\ \dot{\omega}_2 = -\frac{2\omega_1\omega_3}{3} \\ \dot{\omega}_3 = -2\omega_1\omega_2 + \omega_1\omega_3 \tan \vartheta \end{array} \right.$$

$$\text{Pseudo velocities } \left\{ \begin{array}{l} \dot{\vartheta} = \omega_1 \\ \dot{\psi} = \omega_3 \frac{1}{\cos \vartheta} \\ \dot{\varphi} = \omega_2 - \omega_3 \tan \vartheta \end{array} \right.$$

$$\text{Kinematic constraints } \left\{ \begin{array}{l} \dot{x}_G = \omega_1 R \sin \psi \cos \vartheta + \omega_2 R \cos \psi \\ \dot{y}_G = -\omega_1 R \cos \psi \cos \vartheta + \omega_2 R \sin \psi \end{array} \right.$$

Mechanical model



Equations of motion

Essential motion

$$\begin{cases} \dot{\omega}_1 = \frac{6\omega_2\omega_3}{5} - \frac{\omega_3^2 \tan \vartheta}{5} + \frac{4g \sin \vartheta}{5R} \\ \dot{\omega}_2 = -\frac{2\omega_1\omega_3}{3} \\ \dot{\omega}_3 = -2\omega_1\omega_2 + \omega_1\omega_3 \tan \vartheta \\ \dot{\vartheta} = \omega_1 \end{cases}$$

Hidden (cyclic) motion

$$\begin{cases} \dot{\psi} = \omega_3 \frac{1}{\cos \vartheta} \\ \dot{\phi} = \omega_2 - \omega_3 \tan \vartheta \\ \dot{x}_G = \omega_1 R \sin \psi \cos \vartheta + \omega_2 R \cos \psi \\ \dot{y}_G = -\omega_1 R \cos \psi \cos \vartheta + \omega_2 R \sin \psi \end{cases}$$

Steady state motion \leftrightarrow Fixed point of the essential motion

States:

$$\mathbf{x} = [\omega_1 \quad \omega_2 \quad \omega_3 \quad \vartheta \quad \psi \quad \phi \quad x_G \quad y_G]^\top$$

Essential motion:

$$\begin{cases} \dot{\omega}_1 = \frac{6\omega_2\omega_3}{5} - \frac{\omega_3^2 \tan \vartheta}{5} + \frac{4g \sin \vartheta}{5R} \\ \dot{\omega}_2 = -\frac{2\omega_1\omega_3}{3} \\ \dot{\omega}_3 = -2\omega_1\omega_2 + \omega_1\omega_3 \tan \vartheta \\ \dot{\vartheta} = \omega_1 \end{cases}$$

Equilibrium:

$$\omega_1(t) \equiv 0 \quad \omega_2(t) \equiv \omega_{2*} \quad \omega_3(t) \equiv \omega_{3*} \quad \vartheta(t) \equiv \vartheta_*$$

Relation of the states:

$$6\omega_{2*}\omega_{3*}R - \omega_{3*}^2 R \tan \vartheta_* + 4g \sin \vartheta_* = 0$$

 \updownarrow

$$5\dot{\psi}_*^2 R \sin \vartheta_* \cos \vartheta_* + 6\dot{\psi}_* \dot{\phi}_* R \cos \vartheta_* + 4g \sin \vartheta_* = 0$$

Solution:

- ▶ Straight rolling: $\dot{\psi}_* = 0 \quad \vartheta_* = 0 \quad \dot{\phi}_* \in \mathbb{R}$
- ▶ Turning-rolling: $\dot{\psi}_* \neq 0 \quad \vartheta_* = -\pi/2 \dots \pi/2$

$$\dot{\phi}_* = -\frac{5}{6}\dot{\psi}_* \sin \vartheta_* - \frac{2g \tan \vartheta_*}{3R \dot{\psi}_*}$$

- ▶ Spinning: $\vartheta_* = 0 \quad \dot{\psi}_* \in \mathbb{R} \quad \dot{\phi}_* = 0$
- ▶ (Static : $\vartheta_* = 0 \quad \dot{\psi}_* = 0 \quad \dot{\phi}_* = 0$)

Hidden motion

$$\psi_*(t) = \dot{\psi}_* t + \psi_0,$$

$$\varphi_*(t) = \dot{\varphi}_* t + \varphi_0,$$

$$x_{G^*}(t) = \begin{cases} \left(\frac{\dot{\varphi}_*}{\dot{\psi}_*} + \sin \vartheta_* \right) R \sin(\psi_*(t)) + x_0 & \text{ha } \dot{\psi}_* \neq 0 \\ \dot{\varphi}_* t R \cos \psi_0 + x_0 & \text{ha } \dot{\psi}_* = 0 \end{cases}$$

$$y_{G^*}(t) = \begin{cases} -\left(\frac{\dot{\varphi}_*}{\dot{\psi}_*} + \sin \vartheta_* \right) R \cos(\psi_*(t)) + y_0 & \text{ha } \dot{\psi}_* \neq 0 \\ \dot{\varphi}_* t R \sin \psi_0 + y_0 & \text{ha } \dot{\psi}_* = 0 \end{cases}$$

- ▶ G path: **straight, circle or not moving**

! In case of circular motion: $\dot{\varphi}_* = \dot{\varphi}_*(\vartheta_*, \dot{\psi}_*)!$ ρ_G, ρ_P

Relation of the states:

$$6\omega_{2^*}\omega_{3^*}R - \omega_{3^*}^2 R \tan \vartheta_* + 4g \sin \vartheta_* = 0$$

$$\updownarrow$$

$$5\dot{\psi}_*^2 R \sin \vartheta_* \cos \vartheta_* + 6\dot{\psi}_* \dot{\varphi}_* R \cos \vartheta_* + 4g \sin \vartheta_* = 0$$

Solution:

- ▶ Straight rolling: $\dot{\psi}_* = 0 \quad \vartheta_* = 0 \quad \dot{\varphi}_* \in \mathbb{R}$
- ▶ Turning-rolling: $\dot{\psi}_* \neq 0 \quad \vartheta_* = -\pi/2 \dots \pi/2$

$$\dot{\varphi}_* = -\frac{5}{6}\dot{\psi}_* \sin \vartheta_* - \frac{2g \tan \vartheta_*}{3R \dot{\psi}_*}$$

- ▶ Spinning: $\vartheta_* = 0 \quad \dot{\psi}_* \in \mathbb{R} \quad \dot{\varphi}_* = 0$
- ▶ (Static : $\vartheta_* = 0 \quad \dot{\psi}_* = 0 \quad \dot{\varphi}_* = 0$)

Linear stability analysis

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x}$$

$$\mathbf{x} = \begin{bmatrix} \omega_1 & \omega_2 & \omega_3 & \vartheta & \psi & \varphi & x_G & y_G \end{bmatrix}^T$$

$$\mathbf{A} = \begin{bmatrix} 0 & A_{12} & A_{13} & A_{14} & 0 & 0 & 0 & 0 \\ A_{21} & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ A_{31} & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & A_{53} & A_{54} & 0 & 0 & 0 & 0 \\ 0 & 1 & A_{63} & A_{64} & 0 & 0 & 0 & 0 \\ A_{71} & A_{72} & 0 & 0 & A_{75} & 0 & 0 & 0 \\ A_{81} & A_{82} & 0 & 0 & A_{85} & 0 & 0 & 0 \end{bmatrix}$$

Characteristic polynomial:

$$(\lambda^2 - A_{12}A_{21} - A_{13}A_{31} - A_{14})\lambda^6 = 0$$

Stability

► Straight rolling: $|\dot{\varphi}| > \dot{\varphi}_{\text{crit}} = \sqrt{\frac{g}{3R}}$

► Spinning: $|\dot{\psi}| > \dot{\psi}_{\text{crit}} = \sqrt{\frac{4g}{5R}}$

► Turning-rolling ($|\vartheta_*| < \mathcal{V}$):

$$|\dot{\psi}| < \dot{\psi}_{\text{crit},1} \quad \text{or} \quad \dot{\psi}_{\text{crit},2} < |\dot{\psi}|$$

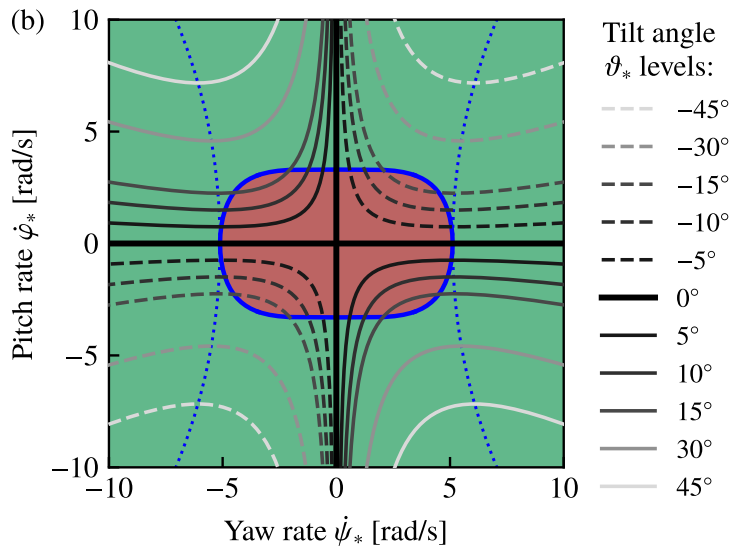
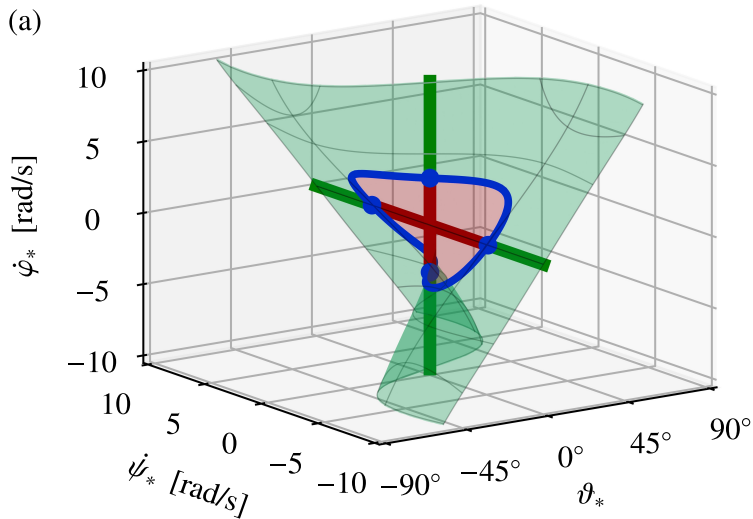
$$\dot{\psi}_{\text{crit},1,2} = \sqrt{\frac{2g}{5R}} \sqrt{\frac{3 - 6 \cos^2 \vartheta_* \pm \sqrt{76 \sin^4 \vartheta_* - 96 \sin^2 \vartheta_* + 9}}{(2 \sin^2 \vartheta_* - 3) \cos \vartheta_*}}$$

Turning always stable if

$$|\vartheta_*| > \mathcal{V} = \arcsin \left(\sqrt{\frac{12}{19} - \frac{9\sqrt{5}}{38}} \right) \approx 18.62^\circ$$

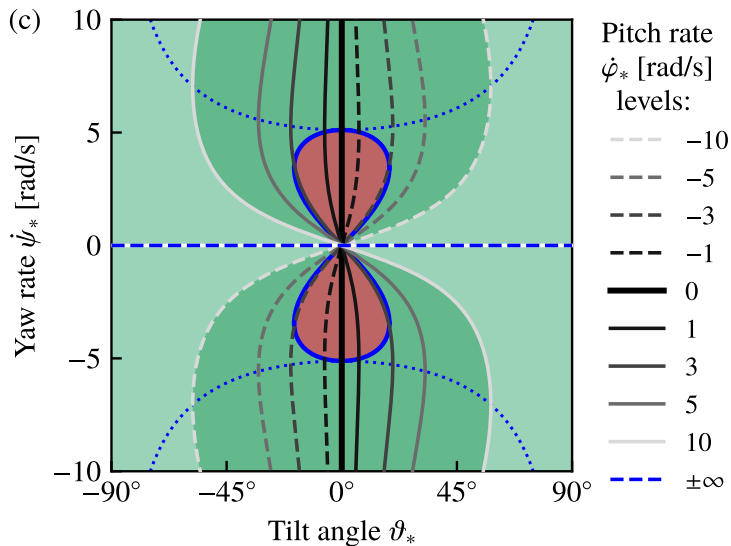
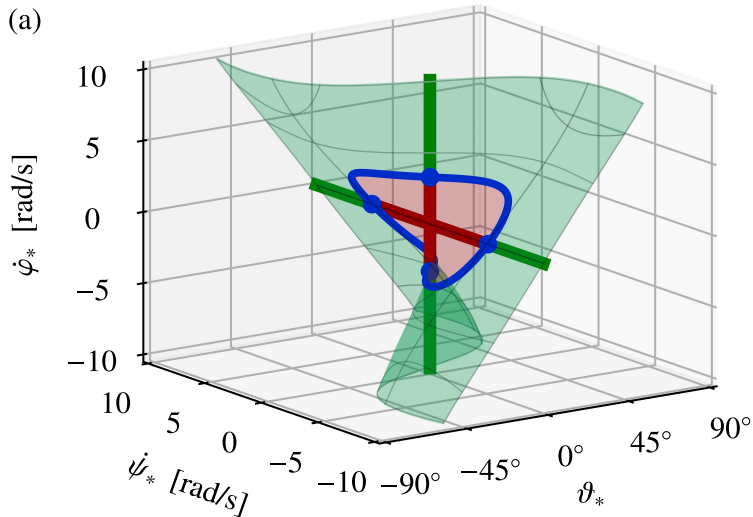
Steady state motion

$$6\omega_{2*}\omega_{3*}R - \omega_{3*}^2R \tan \vartheta_* + 4g \sin \vartheta_* = 0 \leftrightarrow 5\dot{\psi}_*^2R \sin \vartheta_* \cos \vartheta_* + 6\dot{\psi}_*\dot{\varphi}_*R \cos \vartheta_* + 4g \sin \vartheta_* = 0 \rightarrow \dot{\varphi}_*(\vartheta_*, \dot{\psi}_*) = \dots$$



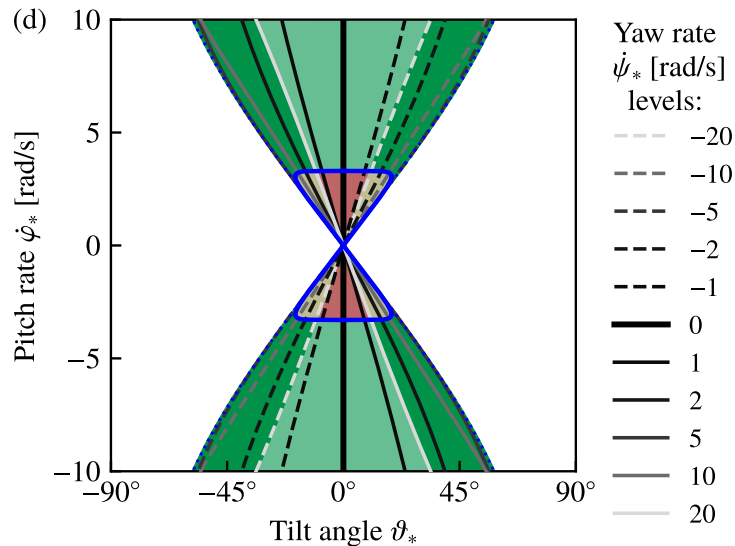
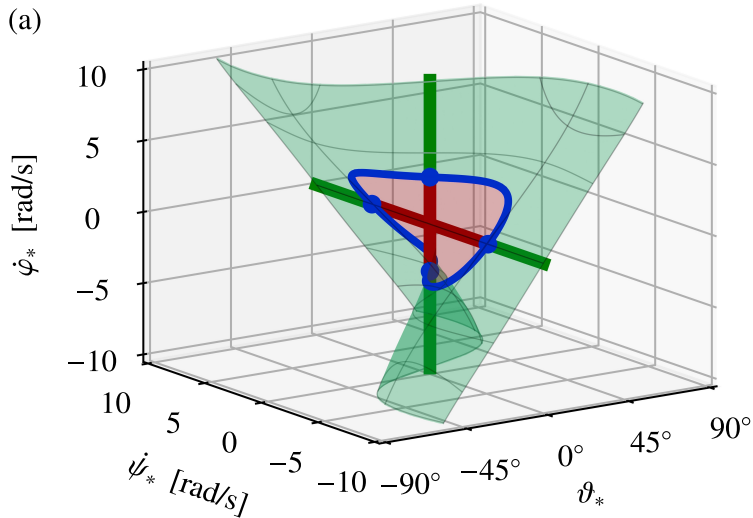
Steady state motion

$$6\omega_{2*}\omega_{3*}R - \omega_{3*}^2R \tan \vartheta_* + 4g \sin \vartheta_* = 0 \leftrightarrow 5\dot{\psi}_*^2R \sin \vartheta_* \cos \vartheta_* + 6\dot{\psi}_*\dot{\phi}_*R \cos \vartheta_* + 4g \sin \vartheta_* = 0 \rightarrow \dot{\phi}_*(\vartheta_*, \dot{\psi}_*) = \dots$$



Steady state motion

$$6\omega_{2*}\omega_{3*}R - \omega_{3*}^2R \tan \vartheta_* + 4g \sin \vartheta_* = 0 \leftrightarrow 5\dot{\psi}_*^2 R \sin \vartheta_* \cos \vartheta_* + 6\dot{\psi}_*\dot{\phi}_*R \cos \vartheta_* + 4g \sin \vartheta_* = 0 \rightarrow \dot{\phi}_*(\vartheta_*, \dot{\psi}_*) = \dots$$



Gyroscopic effect in straight rolling

Using generalized velocities \dot{q} and accelerations \ddot{q} :

$$\frac{5mR^2}{4}\ddot{\vartheta} - \frac{5mR^2}{4}\sin\vartheta\cos\vartheta\dot{\psi}^2 - \frac{3mR^2}{2}\cos\vartheta\dot{\psi}\dot{\varphi} - mgR\sin\vartheta = 0,$$

$$\frac{3mR^2}{2}\ddot{\varphi} + \frac{3mR^2}{2}\sin\vartheta\ddot{\psi} + \frac{5mR^2}{2}\cos\vartheta\dot{\psi}\dot{\vartheta} = 0,$$

$$\frac{mR^2\cos\vartheta}{4}\ddot{\psi} + \frac{mR^2}{2}\dot{\varphi}\dot{\vartheta} = 0.$$

Linearized system: $\vartheta = 0$, $\psi = 0$, $\dot{\varphi} = \dot{\varphi}_*$, $\varphi = \dot{\varphi}_*t$, $\tilde{\varphi} := \dot{\varphi} - \dot{\varphi}_*$

$$\underbrace{\frac{mR^2}{4} \begin{bmatrix} 5 & 0 & 0 \\ 0 & 3 & 0 \\ 0 & 0 & 6 \end{bmatrix}}_{\mathbf{M}} \begin{bmatrix} \ddot{\vartheta} \\ \ddot{\psi} \\ \ddot{\tilde{\varphi}} \end{bmatrix} + \underbrace{\frac{\dot{\varphi}_*mR^2}{2} \begin{bmatrix} 0 & -3 & 0 \\ 3 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}}_{\mathbf{G}} \begin{bmatrix} \dot{\vartheta} \\ \dot{\psi} \\ \dot{\tilde{\varphi}} \end{bmatrix} + \underbrace{mgR \begin{bmatrix} -1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}}_{\mathbf{K}} \begin{bmatrix} \vartheta \\ \psi \\ \tilde{\varphi} \end{bmatrix} = \mathbf{0}$$

Non-smooth effects

- ▶ Lift-off ($N \leq 0$) and/or collision

- ▶ **Dry friction**

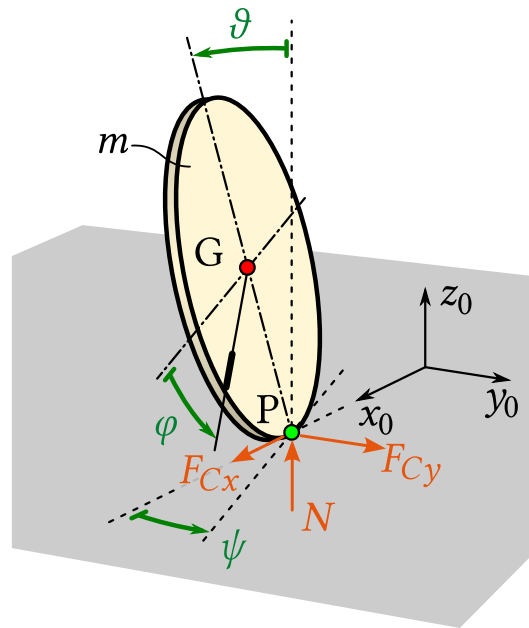
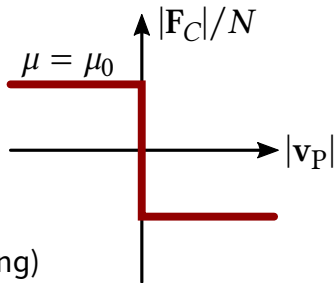
- ▶ Rolling (8 first order ODE, Appell)

$$\omega_1, \omega_2, \omega_3, \vartheta, \psi, \varphi, x_G, y_G$$

- ▶ Sliding (10 first order ODE)

$$\omega_1, \omega_2, \omega_3, \vartheta, \psi, \varphi, x_G, y_G, \dot{x}_G, \dot{y}_G$$

$$F_C \begin{cases} \in [-\mu N, \mu N] & \text{if } \mathbf{v}_P = \mathbf{0} \text{ (rolling)} \\ = -\mu N \frac{\mathbf{v}_P}{|\mathbf{v}_P|} & \text{if } \mathbf{v}_P \neq \mathbf{0} \text{ (sliding)} \end{cases}$$

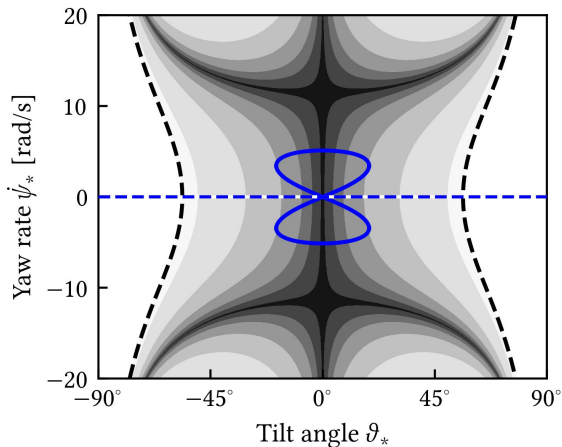
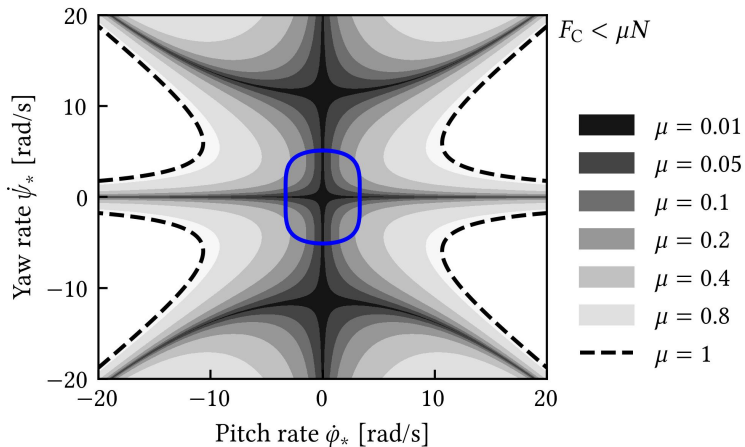
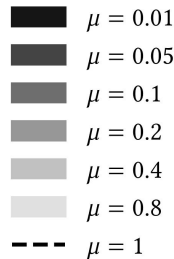
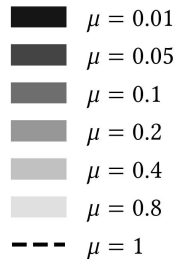


Literature recommendation about 3D rolling: ANTALI, M., STEPAN, G.: Nonsmooth analysis of three-dimensional slipping and rolling in the presence of dry friction. *Nonlinear Dyn* **97**, 1799–1817 (2019).

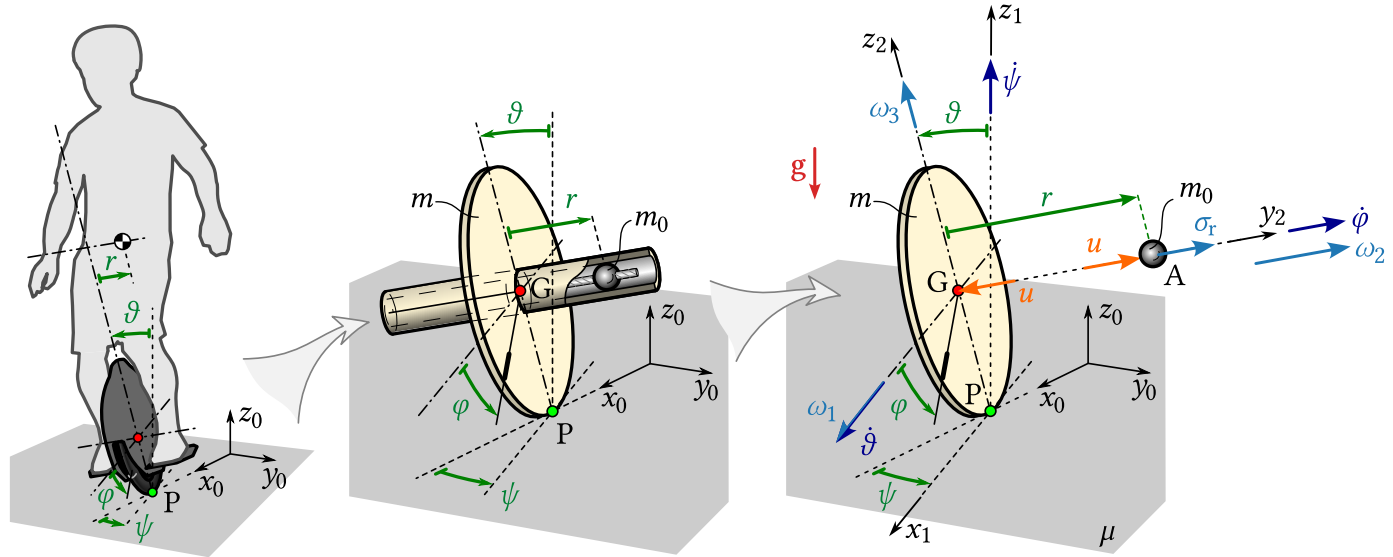
Dry friction and steady states

$$F_C = |\mathbf{F}_C| = \frac{m}{5} |5R\dot{\psi}^2 \sin^3 \vartheta - 4g \sin \vartheta \cos \vartheta + R(6 \sin^2 \vartheta - 1) \dot{\psi} \dot{\phi}|$$

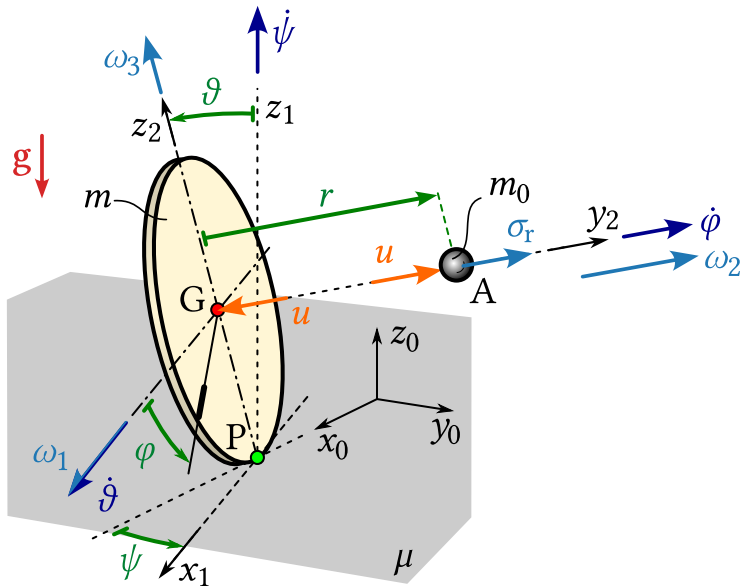
$$N = mg$$

 $F_C < \mu N$  $F_C < \mu N$ 

Unicycle model



Mechanical model



Overview

- ▶ Disc: $m R g$ Point mass: m_0
- ▶ Coordinate frames: $F_0 \xrightarrow{\psi} F_1 \xrightarrow{\vartheta} F_2 \xrightarrow{\varphi} F_3$
- ▶ Generalized coordinates: (6 pcs)
 $x_G \quad y_G \quad \psi \quad \vartheta \quad \varphi \quad r$
- ▶ Pseudo velocities: (4 pcs)
 $\omega_1 := \dot{\vartheta} \quad \omega_2 := \dot{\psi} \sin \vartheta + \dot{\varphi} \quad \omega_3 := \dot{\psi} \cos \vartheta$
 $\sigma := \dot{r} \quad \text{or} \quad \sigma := \dot{r} - \dot{\vartheta} R$
- ▶ States: (10 pcs)

$$\mathbf{x} = [\omega_1 \quad \omega_2 \quad \omega_3 \quad \sigma \quad \vartheta \quad r \quad \psi \quad \varphi \quad x_G \quad y_G]^T.$$

Essential motion with $\sigma := \dot{r}$

$$\dot{\omega}_1 = \frac{1}{5mR^2 + 4m_0r^2} (4\omega_1^2 m_0 R r - \omega_3^2 (mR^2 + 4m_0r^2) \tan \vartheta - 8\omega_1 \sigma m_0 r + \omega_2 \omega_3 (6mR^2 + 4m_0 R r \tan \vartheta) - 4m_0 g r \cos \vartheta + 4m g R \sin \vartheta + 4R u),$$

$$\dot{\omega}_2 = \frac{2}{3mR^2 + 2m_0R^2 + 12m_0r^2} (-2\omega_1 \omega_2 m_0 R r - \omega_1 \omega_3 (mR^2 + m_0R^2 + 4m_0r^2) + 2\omega_3 \sigma m_0 R),$$

$$\dot{\omega}_3 = \frac{1}{3mR^2 + 2m_0R^2 + 12m_0r^2} (-24\omega_3 \sigma m_0 r - \omega_1 \omega_2 (6mR^2 + 4m_0R^2) + \omega_1 \omega_3 ((3mR^2 + 2m_0R^2 + 12m_0r^2) \tan \vartheta + 4m_0 R r)),$$

$$\begin{aligned} \dot{\sigma} = & \frac{m_0}{5mR^2 + 4m_0r^2} (\omega_1^2 (5mR^2 + 4m_0(R^2 + r^2))r - 8\omega_1 \sigma R^2 r \\ & + \omega_3^2 (5mR^2 r - 4m_0 R r^2 \tan \vartheta + 4m_0 r^3 - mR^3 \tan \vartheta) \\ & + \omega_2 \omega_3 R (mR^2 + 4m_0 (R r \tan \vartheta - r^2)) - (mR^2 + 4m_0 r^2) g \sin \vartheta \\ & - 4m_0 g R r \cos \vartheta + (5 \frac{m}{m_0} R^2 + 4R^2 + 4r^2) u), \end{aligned}$$

$$\dot{\vartheta} = \omega_1,$$

$$\dot{r} = \sigma,$$

Essential motion with $\sigma := \dot{r} - \dot{\vartheta}R$

$$\dot{\omega}_1 = \frac{1}{5mR^2 + 4m_0r^2} (-4\omega_1^2 m_0 R r - \omega_3^2 (mR^2 + 4m_0r^2) \tan \vartheta - 8\omega_1 \sigma m_0 r + \omega_2 \omega_3 (6mR^2 + 4m_0 R r \tan \vartheta) - 4m_0 g r \cos \vartheta + 4m g R \sin \vartheta + 4R u),$$

$$\dot{\omega}_2 = \frac{2}{3mR^2 + 2m_0R^2 + 12m_0r^2} (-2\omega_1 \omega_2 m_0 R r + \omega_1 \omega_3 (m_0R^2 - mR^2 - 4m_0r^2) + 2\omega_3 \sigma m_0 R),$$

$$\dot{\omega}_3 = \frac{1}{3mR^2 + 2m_0R^2 + 12m_0r^2} (-24\omega_3 \sigma m_0 r - \omega_1 \omega_2 (6mR^2 + 4m_0R^2) + \omega_1 \omega_3 ((3mR^2 + 2m_0R^2 + 12m_0r^2) \tan \vartheta - 20m_0 R r)),$$

$$\dot{\sigma} = \omega_1^2 r + \omega_3^2 r - \omega_2 \omega_3 R - g \sin \vartheta + \frac{1}{m_0} u,$$

$$\dot{\vartheta} = \omega_1,$$

$$\dot{r} = \sigma + \omega_1 R,$$

Hidden motion (same)

$$\dot{\psi} = \omega_3 \frac{1}{\cos \vartheta},$$

$$\dot{\varphi} = \omega_2 - \omega_3 \tan \vartheta,$$

$$\dot{x}_G = \omega_1 R \sin \psi \cos \vartheta + \omega_2 R \cos \psi, \quad \text{or} \quad \dot{x}_p = \omega_2 R \cos \psi - \omega_3 R \tan \vartheta \cos \psi,$$

$$\dot{y}_G = -\omega_1 R \cos \psi \cos \vartheta + \omega_2 R \sin \psi, \quad \text{or} \quad \dot{y}_p = \omega_2 R \sin \psi - \omega_3 R \tan \vartheta \sin \psi.$$

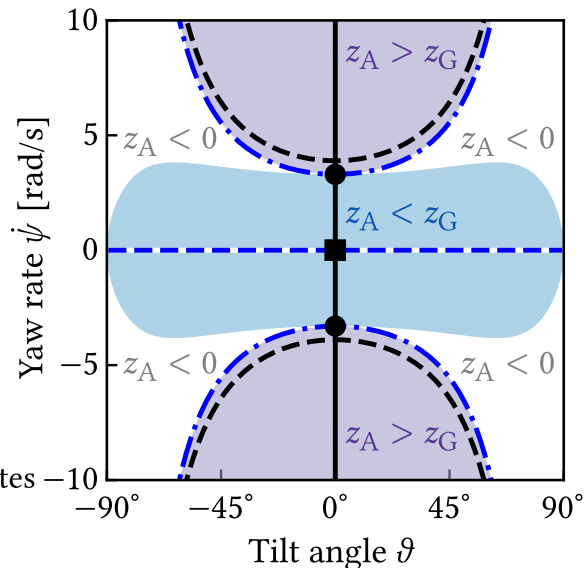
Steady state motion

$$\left. \begin{aligned} \dot{\psi}_*^2 (-4m_0 R r_* \sin^2 \vartheta_* + (-5mR^2 + 4m_0 r_*^2) \sin \vartheta_* \cos \vartheta_*) + \dots \\ \dot{\psi}_*^2 (4m_0 R \sin \vartheta_* \cos \vartheta_* - 4m_0 r_* \cos^2 \vartheta_*) + 4R \dot{\psi}_* \dot{\varphi}_* m_0 \cos \vartheta_* + 4m_0 g \sin \vartheta_* \end{aligned} \right\} \rightarrow \begin{aligned} \dot{\varphi}_*(\vartheta_*, \dot{\psi}_*) = \dots \\ r_*(\vartheta_*, \dot{\psi}_*) = \dots \end{aligned}$$

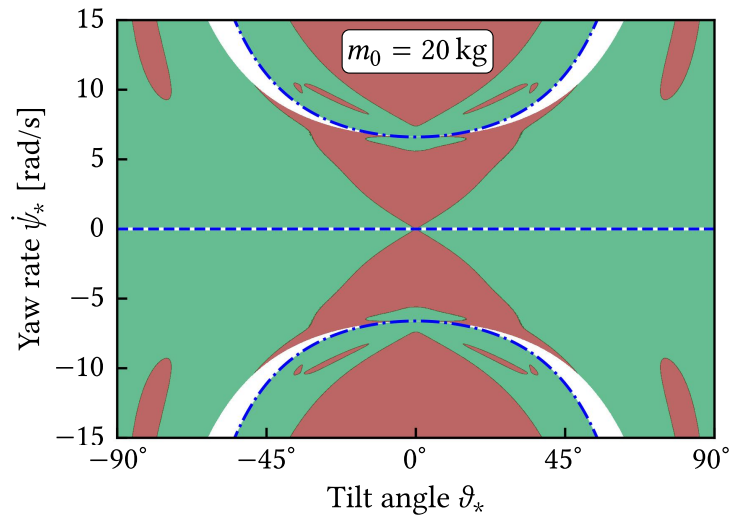
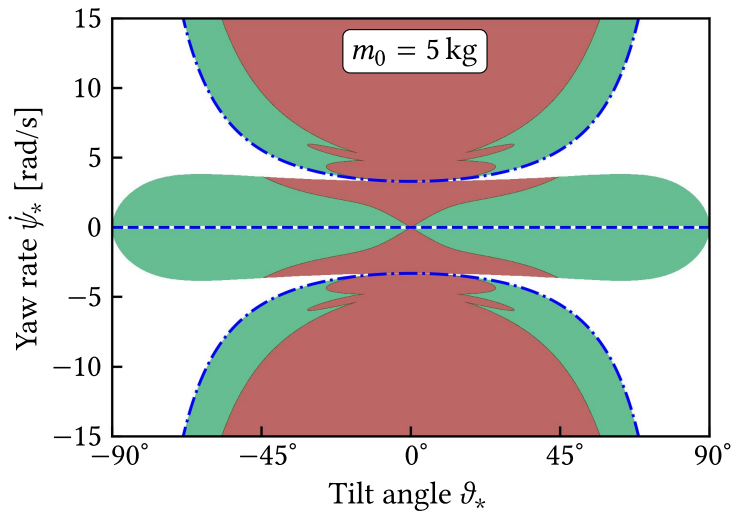
Types:

- ▶ **Straight rolling:** Stability: $|\dot{\varphi}| > \dot{\varphi}_{\text{crit}} = \sqrt{g/(2R)}$
 - ▶ Turning-rolling: Stability: *numerically*
 - ▶ Vertical spinning: Stability: $|\dot{\psi}| \leq \dots$
 - ▶ (Static: *Unstable*)
 - ▶ Tilted spinning: Stability: *numerically*
 - ▶ Vertical turning: Stability: *analytically*
- ! m_0 may go below the ground !

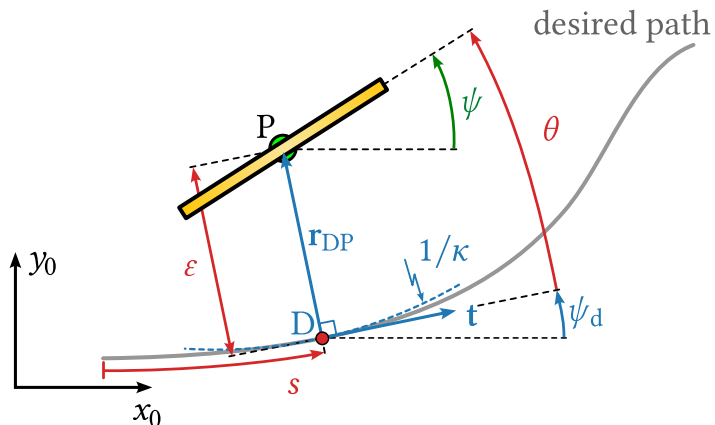
- | | |
|---|--|
| — Non-tilted spinning | - - - Tilted spinning |
| ■ Straight rolling | ● Non-tilted turning |
| ■ Feasible steady states | □ Non-feasible steady states |
| - - - $\dot{\varphi}_* \rightarrow \pm\infty$ | - · - $\dot{\varphi}_*, r_* \rightarrow \pm\infty$ |



Stability of the steady state motion

 $m = 10 \text{ kg}$ $R = 0.3 \text{ m}$ 

Path-following problem



Desired path:

- Curvature $\kappa(s)$

Coordinate transform: $x_P, y_P, \psi \rightarrow s, \varepsilon, \theta$

$$\dot{s} = \frac{1}{1 - \kappa\varepsilon} (\omega_2 R \cos \theta - \omega_3 R \cos \theta \tan \vartheta)$$

$$\dot{\varepsilon} = \omega_2 R \sin \theta - \omega_3 R \sin \theta \tan \vartheta$$

$$\dot{\theta} = \frac{-1}{(1 - \kappa\varepsilon) \cos \vartheta} (\omega_2 R \kappa \cos \theta \cos \vartheta - \omega_3 (1 - \kappa\varepsilon + R \kappa \sin \vartheta \cos \theta))$$

Linear state space model

Based on straight rolling steady state: $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}u$

$$\dot{\omega}_1 = \frac{6}{5}\omega_3\dot{\varphi}_* + \frac{4g}{5R}\vartheta - \frac{4m_0g}{5mR^2}r + \frac{4}{5mR}u,$$

$$\dot{\hat{\omega}}_2 = 0,$$

$$\dot{\omega}_3 = -2\omega_1\dot{\varphi}_*,$$

$$\dot{\sigma} = -\omega_3\dot{\varphi}_*R - g\vartheta + \frac{1}{m_0}u,$$

$$\dot{\vartheta} = \omega_1,$$

$$\dot{r} = \omega_1R + \sigma,$$

$$\dot{\psi} = \omega_3,$$

$$\dot{\varphi} = \hat{\omega}_2 + \dot{\varphi}_*,$$

$$\dot{x}_p = \hat{\omega}_2R \cos \psi_* - \dot{\varphi}_*R\hat{\psi} \sin \psi_* + \dot{\varphi}_*R \cos \psi_*,$$

$$\dot{y}_p = \hat{\omega}_2R \sin \psi_* + \dot{\varphi}_*R\hat{\psi} \cos \psi_* + \dot{\varphi}_*R \sin \psi_*,$$

$$\dot{s} = \hat{\omega}_2R + \dot{\varphi}_*R,$$

$$\dot{\varepsilon} = \dot{\varphi}_*R\theta,$$

$$\dot{\theta} = \omega_3.$$

$$\mathbf{x} = \begin{bmatrix} \omega_1 & \hat{\omega}_2 & \omega_3 & \sigma & \vartheta & r & \hat{\varphi} & \hat{s} & \varepsilon & \theta \end{bmatrix}^T$$

$$\mathbf{A} = \begin{bmatrix} 0 & 0 & \frac{6}{5}\dot{\varphi}_* & 0 & \frac{4g}{5R} & -\frac{4m_0g}{5mR^2} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ -2\dot{\varphi}_* & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -R\dot{\varphi}_* & 0 & -g & 0 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ R & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & R & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & R\dot{\varphi}_* \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$\mathbf{B} = \begin{bmatrix} \frac{4}{5mR} & 0 & 0 & \frac{1}{m_0} & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}^T$$

Not controllable: $\text{Rank}([\mathbf{B} \ \mathbf{A}\mathbf{B} \ \dots \ \mathbf{A}^9\mathbf{B}]) = 6$

Reduced model for steering

- Reduced states: $\tilde{\mathbf{x}} = [\omega_1 \ \sigma \ \vartheta \ r \ \varepsilon \ \theta]^\top$

$$\dot{\omega}_1 = \left(-\frac{12\dot{\varphi}_*^2}{5} + \frac{4g}{5R} \right) \vartheta - \frac{4m_0g}{5mR^2} r + \frac{4}{5mR} u$$

$$\dot{\sigma} = (2R\dot{\varphi}_*^2 - g) \vartheta + \frac{1}{m_0} u$$

$$\dot{\vartheta} = \omega_1$$

$$\dot{r} = \sigma + \omega_1 R$$

$$\dot{\varepsilon} = \dot{\varphi}_* R \theta$$

$$\dot{\theta} = -2\dot{\varphi}_* \vartheta$$

- Control input: $u := \mathbf{K}(\tilde{\mathbf{x}} - \tilde{\mathbf{x}}_{\text{des}})$

$$\mathbf{K} = [D_\vartheta \ D_\sigma \ P_\vartheta \ P_r \ P_\varepsilon \ P_\theta]$$

- Pole placement, Ackermann formula, $\lambda_i := -8$

$$\tilde{\mathbf{x}} = [\omega_1 \ \sigma \ \vartheta \ r \ \varepsilon \ \theta]^\top$$

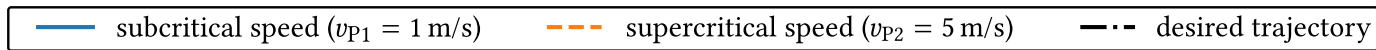
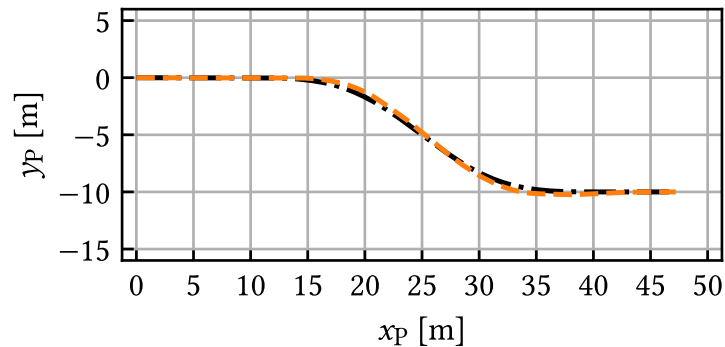
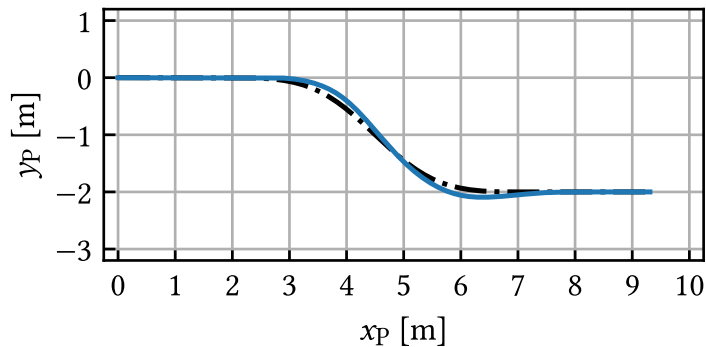
$$\tilde{\mathbf{A}} = \begin{bmatrix} 0 & 0 & \frac{-12\dot{\varphi}_*^2 R + 4g}{5R} & -\frac{4m_0g}{5mR^2} & 0 & 0 \\ 0 & 0 & 2\dot{\varphi}_*^2 R - g & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 \\ R & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & R\dot{\varphi}_* \\ 0 & 0 & -2\dot{\varphi}_* & 0 & 0 & 0 \end{bmatrix}$$

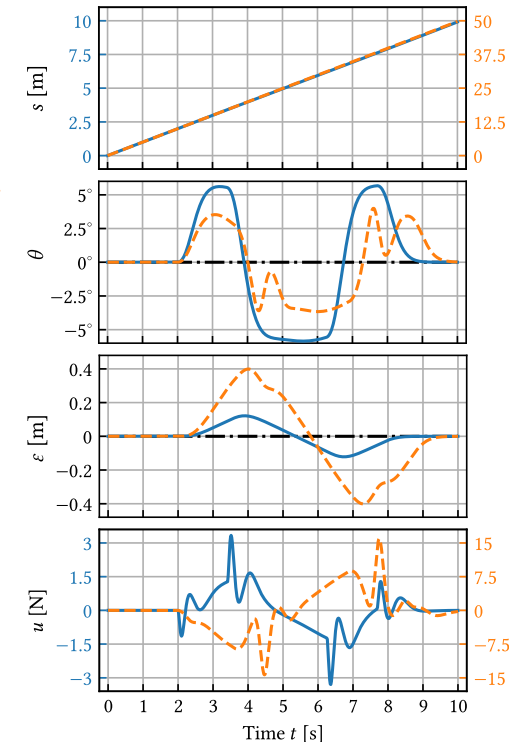
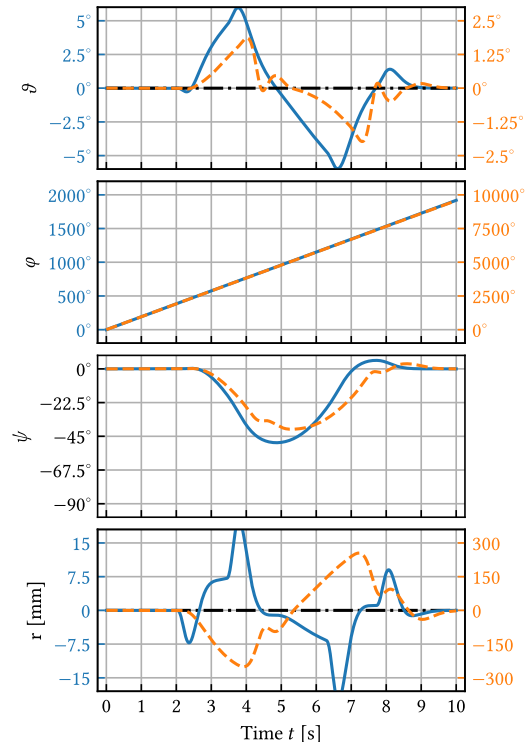
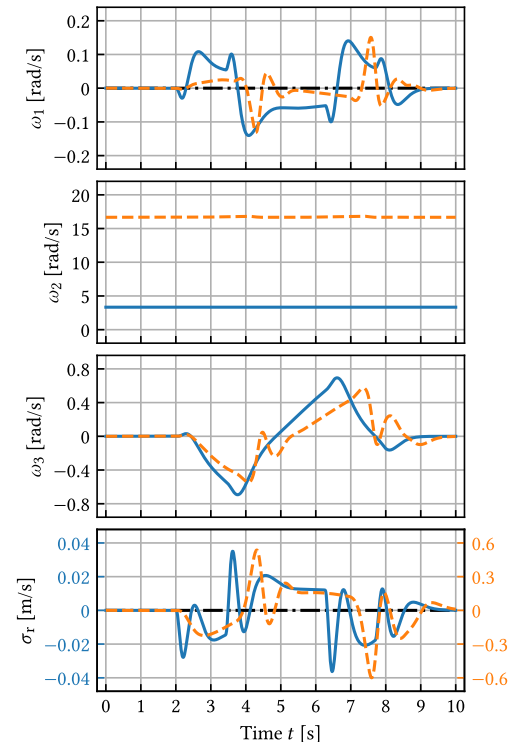
$$\tilde{\mathbf{B}} = \begin{bmatrix} \frac{4}{5mR} & \frac{1}{m_0} & 0 & 0 & 0 & 0 \end{bmatrix}^\top$$

- Controllable:** $\text{Rank}([\tilde{\mathbf{B}} \ \tilde{\mathbf{A}}\tilde{\mathbf{B}} \ \dots \ \tilde{\mathbf{A}}^5\tilde{\mathbf{B}}]) = 6$
- Everything depends on $\dot{\varphi}_* (\neq 0)$!
- Sub-or supercritical speed?

$$|\dot{\varphi}_*| \leq \dot{\varphi}_{\text{crit}} = \sqrt{g/(2R)}$$

Maneuver: Lane change





— subcritical speed ($v_{p1} = 1$ m/s) - - - supercritical speed ($v_{p2} = 5$ m/s) - - - desired trajectory

Non-smooth effects

- ▶ Lift-off ($N \leq 0$) of the wheel
- ▶ Collision of axle (point mass) and ground

- ▶ **Dry friction**

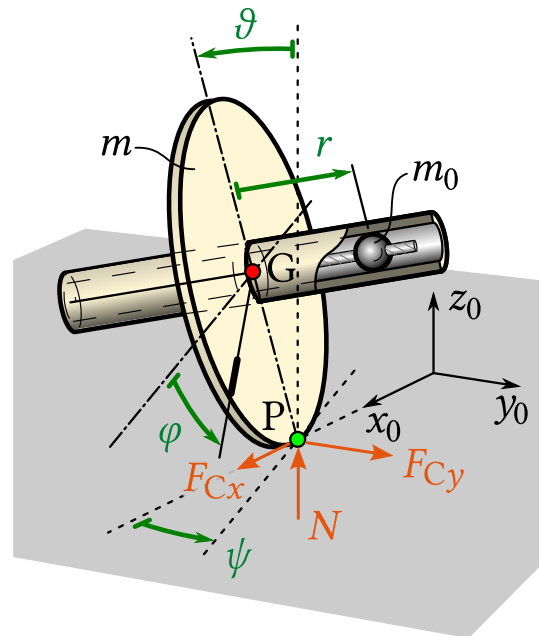
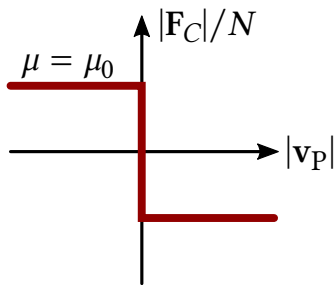
- ▶ Rolling (10 first order ODE, Appell)

$$\omega_1, \omega_2, \omega_3, \vartheta, \sigma, r, \psi, \varphi, x_G, y_G$$

- ▶ Sliding (12 first order ODE)

$$\omega_1, \omega_2, \omega_3, \vartheta, \sigma, r, \psi, \varphi, x_G, y_G, \dot{x}_G, \dot{y}_G$$

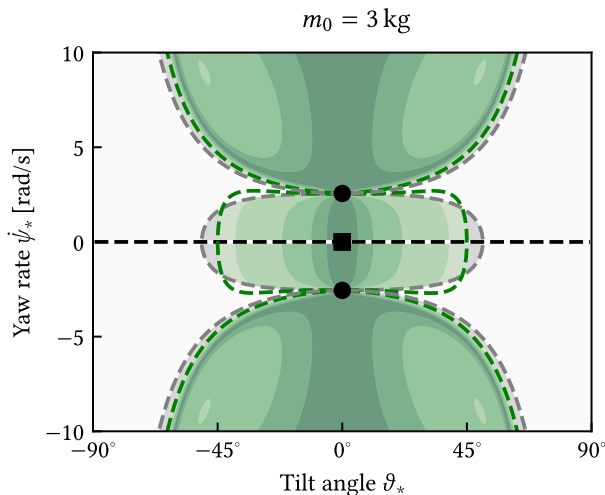
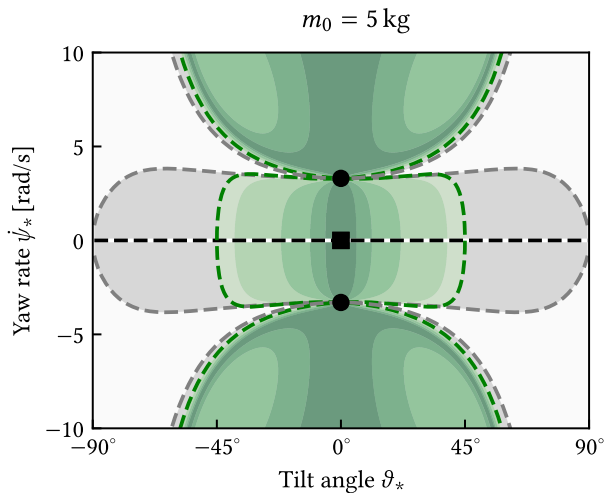
$$F_C \begin{cases} \in [-\mu N, \mu N] & \text{if } \mathbf{v}_P = \mathbf{0} \text{ (rolling)} \\ = -\mu N \frac{\mathbf{v}_P}{|\mathbf{v}_P|} & \text{if } \mathbf{v}_P \neq \mathbf{0} \text{ (sliding)} \end{cases}$$



Dry friction and steady states

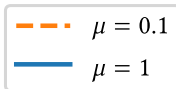
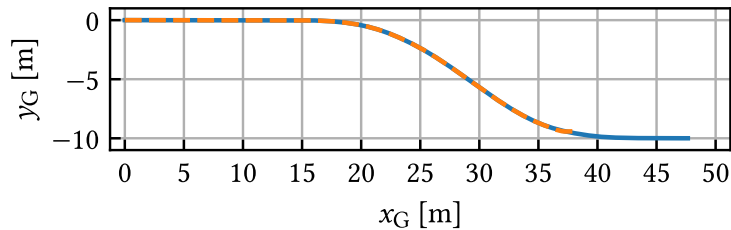
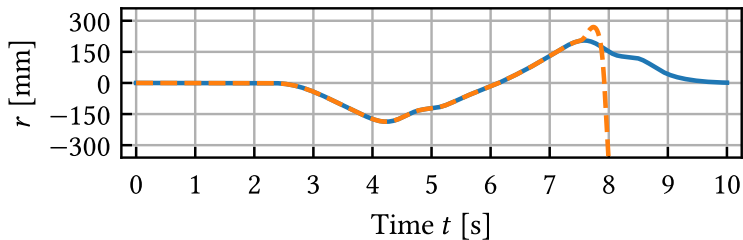
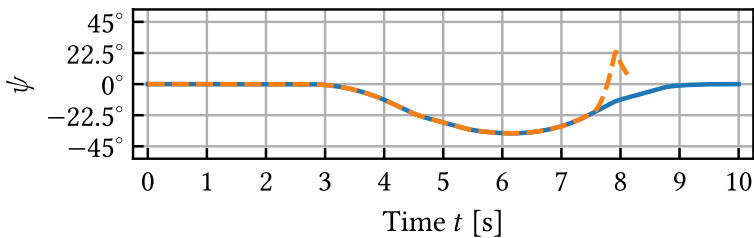
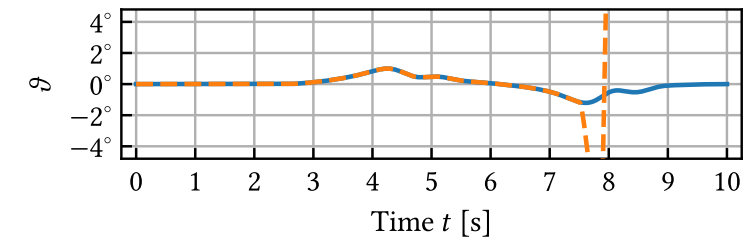
$$F_C = |\mathbf{F}_C| = \dots$$

$$N = \dots$$



- Straight rolling
- Non-tilted turning
- - - $\dot{\psi}_* \rightarrow \pm\infty$
- - - Axle collision
- m_0 below ground
- m_0 above ground
- $\mu = 0.1, F_C < \mu N$
- $\mu = 0.2, F_C < \mu N$
- $\mu = 0.4, F_C < \mu N$
- $\mu = 0.8, F_C < \mu N$
- $\mu = 1, F_C < \mu N$
- - - $\mu = 1$

Maneuver: Lane change



Thank you for your attention!