Selected Newton's methods in computational elasto-plasticity

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Outline and aims of the talk

O Abstract system of non-linear equations inspired by elasto-plasticity.

- to explain selected features of elasto-plastic problems within algebraic level
- specify assumptions for different type of elasto-plastic models

Semismooth Newton method, its modifications and convergence analysis.

- survey of selected Newton-like methods used in elasto-plasticity
- illustration of convergence results on numerical examples
- Oetermination of the limit load in perfect plasticity.
 - important framework for solvability analysis and stability assessment of structures
 - advanced continuation method and related Newton-like solver
- Brief notes to slope stability assessment.
 - overview of finite element methods on stability analysis
 - illustrative examples from geotechnical practice

1. Abstract system of non-linear equations inspired by elasto-plasticity

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Elasto-plastic system of equations

Elasto-plastic problem in terms of displacement after time and space discretization:

find
$$u_h^* \in V_h$$
: $\int_{\Omega} T(e(u_h^*)) : e(v_h) dx = b(v_h) \quad \forall v_h \in V_h,$
 $V_h \subset \{ v \in H^1(\Omega; \mathbb{R}^3) \mid v = 0 \text{ on } \Gamma_D \}, \quad e(v) = \frac{1}{2} \left(\nabla v + (\nabla v)^T \right).$

Investigated example of the stress-strain operator T – the von Mises model:

$$T(e) = \frac{1}{3}(3\lambda + 2\mu)(tr e)I + (1 - \alpha)2\mu e^{D} + \alpha j(2\mu|e^{D}|)\frac{e^{D}}{|e^{D}|}, \qquad j(z) = \begin{cases} z, & z \leq \gamma \\ \gamma, & z \geq \gamma \end{cases}$$

j - continuous, piecewise linear scalar function, switch between elasticity and plasticity $\alpha \in (0, 1)$ - hardening parameter, $\alpha = 0$ - linear elasticity, $\alpha = 1$ - elastic-perfectly plasticity

Nonlinear system of equations in \mathbb{R}^n :

find
$$u^* \in \mathbb{R}^n$$
: $F(u^*) = b$, $F: \mathbb{R}^n \to \mathbb{R}^n$, $b \in \mathbb{R}^n$

$$F(v)^T w := \int_{\Omega} T(e(v_h)) : e(w_h) dx \quad \forall v_h, w_h \in V_h,$$

Properties of F depend on properties of T.

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Basic properties of elasto-plastic functions

(\mathcal{A}_1) F is Lipschitz continuous in \mathbb{R}^n .

- F is almost everywhere differentiable in \mathbb{R}^n , there exists a generalized derivative of F.
- There exists $F^o: \mathbb{R}^n \to \mathbb{R}^{n \times n}$ such that $F^o(u) = F'(u)$ for almost all $u \in \mathbb{R}^n$.
- $F^{o}(u) \in \partial F(u)$ subdifferential in Clarke's sense

(\mathcal{A}_2) F is strongly semismooth in \mathbb{R}^n :

$$\begin{aligned} \forall u \in \mathbb{R}^n, \ \exists L_u, \epsilon_u > 0: \quad \|F(v) - F(u) - F^{\circ}(v)(v-u)\| \leq L_u \|u-v\|^2 \quad \forall v \in B(u; \epsilon_u), \\ F(v) - F(u) &= \int_0^1 F^{\circ}(u + \theta(v-u))(v-u) \, d\theta \qquad \forall u, v \in \mathbb{R}^n. \end{aligned}$$

- Continuous piecewise linear functions are strongly semismooth with $L_u = 0$.
- Smooth functions with locally Lipschitz derivatives are strongly semismooth.
- Finite sums, products or compositions of semismooth functions are again semismooth.
- Implicit function theorem for semismooth functions (E-P operators may be implicit!).



Additional properties for associated plasticity

 (\mathcal{A}_3) F has a convex potential in \mathbb{R}^n with linear growth at infinity, i.e.,

- $\exists \mathcal{I} : \mathbb{R}^n \to \mathbb{R} \text{ (convex)} : \quad \mathcal{I}'(v) = F(v) \quad \forall v \in \mathbb{R}^n,$
- $\exists c_1, c_2 > 0$: $\mathcal{I}(v) \geq c_1 \|v\| c_2 \quad \forall v \in \mathbb{R}^n.$

Consequences:

- F is monotone, i.e. $(F(u) F(v), u v) \ge 0$ for any $u, v \in \mathbb{R}^n$.
- $F^o(v)$ is symmetric and positive semidefinite for any $v \in \mathbb{R}^n$.
- Equivalent minimization problem to $F(u^*) = b$:

$$\mathcal{J}(u^*) \leq \mathcal{J}(v) \ \forall v \in \mathbb{R}^n, \qquad \mathcal{J}(v) = \mathcal{I}(v) - b^\top v.$$

• Sufficient condition for the existence of u^* : $\|b\| < c_1$,

$$[\mathcal{J}(v) \geq (c_1 - \|b\|) \|v\| - c_2 o +\infty$$
 as $\|v\| o +\infty$ (coercivity)]

(A₃) is convenient for E-P models with bounded hardening or perfect plasticity.

Stronger assumptions are available for E-P models with unbounded hardening.



Additional property for plasticity with hardening

 (\mathcal{A}_4) (uniform positive definitness of F^o)

$$\exists \beta_1, \beta_2 > 0: \quad \beta_1 \|v\|^2 \le (F^o(u)v, v) \le \beta_2 \|v\|^2 \quad \forall u, v \in \mathbb{R}^n$$

Consequences:

- Inverses of F^o(u) are also uniformly positive definite.
- F is strongly monotone, i.e. $(F(u) F(v), u v) \ge \beta_1 ||u v||^2$ for any $u, v \in \mathbb{R}^n$.
- \mathcal{J} is strictly convex and coercive in \mathbb{R}^n .
- There exists a unique solution u^* satisfying $F(u^*) = b$

Remarks:

- (A_4) will be considered within convergence analysis in Section 2.
- (A_4) will not be considered within convergence analysis in Section 3.

2. Semismooth Newton method, its modifications and convergence analysis

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Semismooth Newton method

Algorithm:

$$F^{o}(u^{k})(u^{k+1}-u^{k})=b-F(u^{k}), \ k=0,1,\ldots, \ u^{0}-$$
 given,

Local quadratic convergence under the assumptions $(A_1) - (A_4)$:

$$||u^* - u^{k+1}|| = O(||u^* - u^k||^2)$$

Sketch of the proof: if u^k is sufficiently close to u^* then

$$u^{*} - u^{k+1} = u^{*} - u^{k} - F^{o}(u^{k})^{-1} [b - F(u^{k})]$$

= $F^{o}(u^{k})^{-1} [F(u^{k}) - F(u^{*}) - F^{o}(u^{k})(u^{k} - u^{*})]$
 $||u^{*} - u^{k+1}|| \le ||F^{o}(u^{k})^{-1}|| ||F(u^{k}) - F(u^{*}) - F^{o}(u^{k})(u^{k} - u^{*})||$
 $\le \frac{(\mathcal{A}_{2}, \mathcal{A}_{4})}{\beta_{1}} \frac{1}{\mathcal{L}_{u^{*}}} ||u^{*} - u^{k}||^{2}.$

Remark: This result holds for more general assumptions than $(A_1) - (A_4)$, [Qi and Sun 1993]

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Quasi-Newton method and its nonsmooth variant

Algorithm: [Faragó, Karátson 2002], [Karátson, Faragó 2003], [Borsos, Karátson 2022]

$$u^{k+1} := u^k + \frac{2}{M_k + m_k} B_k^{-1}(b - F(u^k))$$
 $k = 0, 1, ..., u^0 - \text{given},$

where $B_k \in \mathbb{R}_{sym}^{n imes n}$, $0 < m_{min} \leq m_k \leq M_k \leq M_{max}$ and

$$m_k(B_kv,v) \leq (F^o(u^k)v,v) \leq M_k(B_kv,v) \quad \forall u,v \in \mathbb{R}^n, \ \forall k \in \mathbb{N}.$$

Original convergence results for smooth operators:

Let $(A_1) - (A_4)$ hold and F has a Lipschitz continuous derivative F'. Then

$$\limsup \frac{\|F(u^{k+1})\|_*}{\|F(u^k)\|_*} \leq \limsup \frac{M_k - m_k}{M_k + m_k} < 1, \qquad \|v\|_* := (F'(u^*)^{-1}v, \, v)^{1/2} + \frac{1}{M_k + m_k} < 1.$$

Remarks:

- only linear convergence, but faster assembling of B_k than $F'(u^k)$
- Examples when the quasi-Newton method is faster than the Newton method: [Borsos, Karátson 2022], in nonlinear elasticity: [Karátson, S., Béreš 2024]
- Recommendation: combination of the quasi-Newton method with deflated CG method

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Quasi-Newton method and its nonsmooth variant

Local linear convergence for non-smooth operators I: Let $(A_1) - (A_4)$ hold. Then

$$||u^* - u^{k+1}|| \le \frac{\beta_2}{\beta_1} \frac{M_k - m_k}{M_k + m_k} ||u^* - u^{k+1}|| + O(||u^* - u^{k+1}||^2).$$

$$\text{criterion:} \quad \frac{\beta_2}{\beta_1} \frac{M_k - m_k}{M_k + m_k} \leq q < 1 \quad \forall k \in \mathbb{R}^n, \qquad \text{however} \quad \frac{\beta_2}{\beta_1} > 1$$

Sketch of the proof: if u^k is sufficiently close to u^* then

$$u^{*} - u^{k+1} = \left(I - \frac{2}{M_{k} + m_{k}} B_{k}^{-1} F^{o}(u_{k})\right) (u^{*} - u^{k}) + \frac{2}{M_{k} + m_{k}} B_{k}^{-1} \left[F(u^{k}) - F(u^{*}) - F^{o}(u^{k})(u^{k} - u^{*})\right],$$
$$\|u^{*} - u^{k+1}\| \stackrel{(A_{2}, A_{4})}{\leq} \left\|I - \frac{2}{M_{k} + m_{k}} B_{k}^{-1} F^{o}(u_{k})\right\| \|u^{*} - u^{k}\| + O(\|u^{*} - u^{k}\|^{2}),$$

$$\left\|I - \frac{2}{M_k + m_k} B_k^{-1} F^{\circ}(u_k)\right\| \leq \left\|F^{\circ}(u_k)^{-1} - \frac{2}{M_k + m_k} B_k^{-1}\right\| \|F^{\circ}(u_k)\| \stackrel{(\mathcal{A}_4)}{\leq} \frac{\beta_2}{\beta_1} \frac{M_k - m_k}{M_k + m_k}.$$

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Quasi-Newton method and its nonsmooth variant

Local linear convergence for non-smooth operators II: Let $(\mathcal{A}_1)-(\mathcal{A}_4)$ hold. Then

$$\|u^* - u^{k+1}\|_{u^*} \leq \sqrt{\frac{\gamma_{2,k}}{\gamma_{1,k}}} \frac{M_k - m_k}{M_k + m_k} \|u^* - u^{k+1}\|_{u^*} + O(\|u^* - u^{k+1}\|_{u^*}^2),$$

where

$$\begin{aligned} \|v\|_{u^*} &:= \sqrt{(F^o(u^*)v, v)}, \quad \|v\|_{u^k} = \sqrt{(F^o(u^k)v, v)} \quad \forall u, v \in \mathbb{R}^n, \\ \gamma_{1,k} \|v\|_{u^*}^2 &\leq \|v\|_{u^k}^2 \leq \gamma_{2,k} \|v\|_{u^*}^2 \quad \forall u, v \in \mathbb{R}^n, \ \forall k \in \mathbb{N}, \ \gamma_{1,k} \geq \gamma_{min} > 0 \end{aligned}$$

criterion:
$$\sqrt{\frac{\gamma_{2,k}}{\gamma_{1,k}}} \frac{M_k - m_k}{M_k + m_k} \le q < 1 \quad \forall k \in \mathbb{N},$$
 realistic assumption: $\sqrt{\frac{\gamma_{2,k}}{\gamma_{1,k}}} \approx 1$

Sketch of the proof: if u^k is sufficiently close to u^* then

$$\|u^{*} - u^{k+1}\|_{u^{k}} \overset{(\mathcal{A}_{2}, \mathcal{A}_{4})}{\leq} \|I - \frac{2}{M_{k} + m_{k}} B_{k}^{-1} F^{o}(u_{k})\|_{u^{k}} \|u^{*} - u^{k}\|_{u^{k}} + O(\|u^{*} - u^{k}\|_{u^{k}}^{2}),$$

$$\|I - \frac{2}{M_{k} + m_{k}} B_{k}^{-1} F^{o}(u_{k})\|_{u^{k}} \leq \frac{M_{k} - m_{k}}{M_{k} + m_{k}}, \quad \frac{\|u^{*} - u^{k+1}\|_{u^{k}}}{\|u^{*} - u^{k+1}\|_{u^{*}}} \geq \sqrt{\gamma_{1,k}}, \quad \frac{\|u^{*} - u^{k}\|_{u^{k}}}{\|u^{*} - u^{k}\|_{u^{*}}} \leq \sqrt{\gamma_{2,k}}$$
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Examples of the preconditioners B_k

Quasi-Newton 1: $B_k = K_{elast}$

- elastic stiffness matrix with fixed material parameters
- advantage: a constant matrix with a simple assembling
- disadvantage: poor approximation of $F^o(u^k)$

Quasi-Newton 2: $B_k = K_{elast,k}$

- elastic stiffness matrix with variable material parameters
- advantage: better approximation of $F^o(u^k)$
- disadvantage: assembling in each iteration

Smoothing Newton method: [Qi, Sun 2002] $B_k = F'_{\epsilon}(u^k)$

- F_{ϵ} is a smooth approximation of F
- advantage: M_k and m_k are close to one as $\epsilon
 ightarrow 0$
- disadvantage: assembling of $F'_{\epsilon}(u^k)$ is not faster than assembling of $F^o(u^k)$
- The operator F'_{ϵ} will be used later, within the continuation Newton method.



Numerical example in 3D – strip footing



- 2 investigated values of the hardening: $\alpha = 0.5$ and $\alpha = 0.9$ (stronger nonlinearity)
- 3 investigated meshes with 38 400, 307 200 and 1 036 800 elements
- comparison of the Newton, Quasi-Newton 1 and Quasi-Newton 2 methods
- similar results for smooth version of the E-P problem, see [Karátson, S., Béreš 2024]

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Comparison of iteration numbers



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Comparison of computational times



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Comparison of physical arrays

 $\alpha = 0.5$ $\alpha = 0.9$

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Semismooth Newton method with damping

Algorithm: (used in elasto-plasticity in [S. 2012])

$$u^{k+1} := u^k + \alpha_k s^k \qquad k = 0, 1, \dots, \quad u^0 - \text{ given},$$

$$F^o(u^k)s^k = b - F(u^k)$$

$$\alpha_k = \arg\min_{\omega \in [0,1]} \mathcal{J}(u^k + \omega s^k), \qquad \mathcal{J}'(v) = F(v) - b^\top v$$

Remarks:

- Newton' methods without damping sometimes do not converge in elasto-plasticity
- damping enables to investigate global convergence
- optimization framework simplifies convergence analysis
- alternative line-search based on the Armijo rule: choose α_k satisfying

$$\mathcal{J}(u^k + \alpha_k s^k) - \mathcal{J}(u^k) \leq -\varrho \alpha_k (F^o(u^k) s^k, s^k), \quad \varrho \in (0, 1)$$

• similar convergence analysis for the Armijo line search



Global convergence of the damped method

Algorithm: $u^{k+1} := u^k + \alpha_k s^k$, $F^o(u^k)s^k = b - F(u^k)$, $\alpha_k = \arg \min_{\beta \in [0,1]} \mathcal{J}(u^k + \beta s^k)$ Key estimates derived under the assumptions (\mathcal{A}_1) , (\mathcal{A}_3) and (\mathcal{A}_4) :

$$\begin{split} (\mathcal{J}'(u^k), s^k) &\leq -\beta_1 \|s^k\|^2, \\ \alpha_k &\geq \frac{\beta_1}{\beta_2} > 0, \quad \text{if } s^k \neq 0, \\ \mathcal{J}(u^{k+1}) - \mathcal{J}(u^k) &\leq -\frac{1}{2}\beta_1 \alpha_k^2 \|s^k\|^2 \leq -\frac{\beta_1^3}{2\beta_2^2} \|s^k\|^2, \\ &\sum_{k=0}^{+\infty} \|s^k\|^2 \leq \frac{2\beta_2^2 (\mathcal{J}(u^0) - \mathcal{J}(u^*))}{\beta_1^3} \implies s^k \to 0, \\ &\sum_{k=0}^{+\infty} \|u^* - u^k\|^2 \leq \frac{2\beta_2^4 (\mathcal{J}(u^0) - \mathcal{J}(u^*))}{\beta_1^5} \implies u^k \to u^*. \end{split}$$

Remarks:

- The global convergence result can be extended to infinite dimensional Hilbert spaces.
- Semismoothness of F is not necessary for the global convergence.

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Superlinear convergence of the damped method

Algorithm: $u^{k+1} := u^k + \alpha_k s^k$, $F^o(u^k)s^k = b - F(u^k)$, $\alpha_k = \arg \min_{\beta \in [0,1]} \mathcal{J}(u^k + \beta s^k)$ Key results under the assumptions $(\mathcal{A}_1) - (\mathcal{A}_4)$:

 $\lim_{k\to+\infty}\alpha_k=1$

$$\|u^* - u^{k+1}\| = (1 - \alpha_k)\|u^* - u^k\| + O(\|u^* - u^k\|^2) = o(\|u^* - u^k\|)$$

Remark:

- Semismoothness of F is crucial for local superlinear convergence of the damped method.
- Superlinear convergence of the damped Newton was illustrated on numerical examples.
- Numbers of iteration only slightly depend on mesh density, see [S. 2012].



Continuation Newton method [Axelsson, S. 2015]

Severely nonlinear system of equations with a nonsmooth function:

find $u^* \in \mathbb{R}^n$: $F(u^*) = b$ $F: \mathbb{R}^n \to \mathbb{R}^n$, $b \in \mathbb{R}^n$

Load-based continuation method:

$$F(0) = 0$$
, $F(\hat{u}(t)) = tb$, $0 \le t \le 1$, $\hat{u}(1) = u^*$.

Smooth approximation of F:

$$\{F_{\epsilon}\}_{\epsilon \in (0,\epsilon_0)} - \text{ smooth}: \quad \lim_{\epsilon \to 0} F_{\epsilon}(v) = F(v), \quad \lim_{\epsilon \to 0} F'_{\epsilon}(v) = F^o(v) \ \forall v \in \mathbb{R}^n$$

One-step smoothing Newton method: $0 = t_0 < t_1 < \ldots < t_N = 1$, $\tau_k := t_{k+1} - t_k$

$$F'_{\epsilon}(u^k)(u^{k+1}-u^k) = t_{k+1}b - F(u^k), \ k = 0, 1, \dots N-1, \ u^0 = 0,$$

Aim: find assumptions guaranteeing that u^k is close to $\hat{u}(t_k)$ for any k = 1, ..., N



Assumptions and their consequences

$$(\mathcal{A}_5) \quad \exists M > 0: \quad \|F_{\epsilon}(u) - F(u) - (F_{\epsilon}(v) - F(v))\| \leq M\epsilon \|u - v\| \quad \forall u, v \in \mathbb{R}^n, \ \forall \epsilon \in (0, \epsilon_0).$$

$$(\mathcal{A}_6) \quad \exists L > 0: \quad \|F_{\epsilon}(v) - F_{\epsilon}(u) - F'_{\epsilon}(v)(v-u)\| \leq \frac{L}{2\epsilon} \|u-v\|^2 \quad \forall u, v \in \mathbb{R}^n, \ \forall \epsilon \in (0, \epsilon_0).$$

$$(\mathcal{A}_7) \quad \exists q > 0: \quad \begin{cases} [F(u) - F(v)]^T (u - v) \ge q \|u - v\|^2 & \forall u, v \in \mathbb{R}^n, \\ [F_\epsilon(u) - F_\epsilon(v)]^T (u - v) \ge q \|u - v\|^2 & \forall u, v \in \mathbb{R}^n, \, \forall \epsilon \in (0, \epsilon_0). \end{cases}$$

- Hence: $\|\hat{u}(t_{k+1}) \hat{u}(t_k)\| \le \frac{1}{q} \|F(\hat{u}(t_{k+1})) F(\hat{u}(t_k))\| = \frac{\|b\|}{q} \tau_k \quad \forall k = 0, 1, \dots N-1$
- Hence: $\|[F'_{\epsilon}(u^k)]^{-1}\| \leq \frac{1}{q} \quad \forall k = 1, 2 \dots N$
- If (\mathcal{A}_4) hold then $q = \beta_1$.

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Convergence of the algorithm

Let the assumptions (A_5) , (A_6) , (A_7) hold with the constants M, L and q. Let

$$\epsilon \leq rac{q}{4M}, \quad au_k \leq rac{q^2\epsilon}{4L\|b\|} \quad \forall k = 0, 1, \dots, N-1.$$

Then

$$\|\hat{u}(t_k) - u^k\| \le \frac{\|b\|}{q} \max_{0 \le l \le k-1} \tau_l, \quad k = 0, 1 \dots.$$

Sketch of the proof:

The result can be shown by mathematical induction

$$\hat{u}(t_{k+1}) - u^{k+1} = -(F'_{\epsilon}(u^{k}))^{-1} \left[F(\hat{u}(t_{k+1})) - F_{\epsilon}(\hat{u}(t_{k+1})) - (F(u^{k}) - F_{\epsilon}(u^{k})) \right] \\ + (F'_{\epsilon}(u^{k}))^{-1} \left[F_{\epsilon}(u^{k}) - F_{\epsilon}(\hat{u}(t_{k+1})) - F'_{\epsilon}(u^{k})(u^{k} - \hat{u}(t_{k+1})) \right].$$

Hence:

$$\begin{aligned} \|\hat{u}(t_{k+1}) - u^{k+1}\| &\leq \frac{1}{q} \left[M\epsilon \|\hat{u}(t_{k+1}) - u^k\| + \frac{L}{2\epsilon} \|\hat{u}(t_{k+1}) - u^k\|^2 \right], \\ \|\hat{u}(t_{k+1}) - u^{k+1}\| &\leq \frac{\|b\|}{2q} \tau_k + \left(\frac{1}{4} + \frac{L}{q\epsilon} \|\hat{u}(t_k) - u^k\|\right) \|\hat{u}(t_k) - u^k\|. \end{aligned}$$

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Regularization of the stress-strain operator

Algebraic notation (recalling):

$$\begin{split} F(v)^T w &:= \int_{\Omega} T(e(v_h)) : e(w_h) \, \mathrm{d}x \quad \forall v_h, w_h \in V_h, \\ F_{\epsilon}(v)^T w &:= \int_{\Omega} T_{\epsilon}(e(v_h)) : e(w_h) \, \mathrm{d}x \quad \forall v_h, w_h \in V_h. \end{split}$$

Stress-strain operator and its smooth approximation:

$$T(e) = \frac{1}{3}(3\lambda + 2\mu)(tr e)I + (1 - \alpha)2\mu e^{D} + \alpha j(2\mu|e^{D}|)\frac{e^{D}}{|e^{D}|},$$

$$T_{\epsilon}(e) = \frac{1}{3}(3\lambda + 2\mu)(tr e)I + (1 - \alpha)2\mu e^{D} + \alpha j_{\epsilon}(2\mu|e^{D}|)\frac{e^{D}}{|e^{D}|},$$

 j, j_{ϵ} - nonlinear scalar function and its smooth approximation



The function *j* and its smooth approximation j_{ϵ}

$$j(z) = \begin{cases} z, & z \leq \gamma \\ \gamma, & z \geq \gamma \end{cases}, \qquad j_{\epsilon}(z) := \begin{cases} z, & z \leq \gamma - \epsilon \\ \gamma - \frac{1}{4\epsilon}(z - \gamma - \epsilon)^2, & z \in [\gamma - \epsilon, \gamma + \epsilon] \\ \gamma, & z \geq \gamma + \epsilon \end{cases}$$

Relationships between j and j_{ϵ} implying the assumptions $(\mathcal{A}_5)-(\mathcal{A}_7)$:

$$\begin{aligned} |j(z) - j_{\epsilon}(z)| &\leq \quad \frac{\epsilon}{4} \quad \forall z \in \mathbb{R}, \ \forall \epsilon \in (0, \gamma), \\ |j(z_1) - j(z_2) - j_{\epsilon}(z_1) + j_{\epsilon}(z_2)| &\leq \quad \frac{\epsilon}{2} |z_1 - z_2| \quad \forall z_1, z_2 \in \mathbb{R}, \ \forall \epsilon > 0, \\ |j_{\epsilon}(z_2) - j_{\epsilon}(z_1) - j'_{\epsilon}(z_2)(z_2 - z_1)| &\leq \quad \frac{1}{4\epsilon} (z_1 - z_2)^2 \quad \forall z_1, z_2 \in \mathbb{R}, \ \forall \epsilon > 0 \end{aligned}$$

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Assumptions $(A_5)-(A_7)$ for the E-P operators

$$\begin{split} (1-\alpha)\|v\|_{e}^{2} &\leq v^{T}K_{\epsilon}'(w)v \leq \|v\|_{e}^{2} \quad \forall v, w \in \mathbb{R}^{n}, \ \forall \epsilon \in (0,\epsilon_{0}), \\ v^{T}(F(w+v)-F(w)) \geq (1-\alpha)\|v\|_{e}^{2} \quad \forall v, w \in \mathbb{R}^{n}, \\ \|F(v)-F(w)-K_{\epsilon}(v)+K_{\epsilon}(w)\|_{*} &\leq M\epsilon\|v-w\|_{e} \quad \forall v, w \in \mathbb{R}^{n}, \ \forall \epsilon \in (0,\epsilon_{0}), \\ \|K_{\epsilon}(v)-K_{\epsilon}(u)-K_{\epsilon}'(v)(v-u)\|_{*} &\leq \frac{L}{2\epsilon}\|v-w\|_{e,L^{4}}^{2} \quad \forall u, w \in S, \ \forall \epsilon \in (0,\epsilon_{0}), \end{split}$$

where

$$\|v\|_e, \|v\|_{e,L^4} - \text{energy norms}, \quad \|v\|_* := \sup_{w \in \mathbb{R}^n, \|w\|_e = 1} |v^T w| \quad \forall v \in \mathbb{R}^n.$$

Remarks:

- The estimates are dependent on the hardening parameter α .
- The estimates are independent of the discretization parameter.
- The convergence result could be extended to the functional setting, unlike $\epsilon \rightarrow 0$.



Numerical example



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Numerical results - comparison of solution paths

$$F(\hat{u}(t_k)) = t_k b, \quad u^k = u^{k-1} + (F'_{\epsilon}(u^{k-1}))^{-1}[t_k b - F(u^{k-1})]$$

Comparison of exact solution path $\{\hat{u}(t)\}_{t\in[0,1]}$ with its approximation $\{u^k\}_{k=0}^N$:

- the quantity $b^{\top} \hat{u}(t)$ is used for the visualization, where b is r.h.s
- the curves almost coincide with the exception of $t \in (0.45, 0.55)$
- linear elastic branch for $t \le 0.45$, hardening branch of the curve for $t \in (0.55, 1)$



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Numerical results – convergence of the algorithm

Dependence of $\|\hat{u}(t_k) - u^k\|_e$ on $\tau = t_k - t_{k-1} = const.$:

- error measure is minimal for $t \in [0, 0.45]$ and $t \in [0.55, 1]$
- error measure tends to zero as au
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3. Determination of the limit load in perfect plasticity by Newton-like methods

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Elastic-perfectly plastic problem and limit load

About the elastic-perfectly plastic problem:

- $T(e) = \frac{1}{3}(3\lambda + 2\mu)(tr e)I + (1 \alpha)2\mu e^{D} + \alpha j(2\mu|e^{D}|)\frac{e^{D}}{|e^{D}|}, \quad \alpha = 1.$
- Assumptions $(A_1) (A_3)$ hold (F is semismooth and has a potential with linear growth).
- Assumption (A₄) does not hold (F is not strongly monotone).
- Problem $F(u^*) = b$ has the solution u^* only for sufficiently small b.

Problem parametrization and the limit load:

- $F(\hat{u}(t)) = tb$, $t \ge 0$, t is a scalar load factor
- t_{lim} limit load factor = supremum of t for which $\hat{u}(t)$ exists.
- t_{lim} important for safety assessment of structures.
- Solution exists for any $t \in [0, t_{lim})$, but is unbounded in vicinity of t_{lim} .
- Continuation over t is not too numerically stable.



Advanced continuation technique for finding t_{lim}

Energy-based control the loading path:

- Idea: use the dependence between t and $b^{ op} \hat{u}(t)$ and its inverse
- [S., Haslinger, Hlaváček, Čermák 2015], [S., Haslinger, Reddy, Repin 2021]



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Advanced continuation method and limit analysis

Nonlinear system with additional equation:

find $\bar{u}(\omega) \in \mathbb{R}^n$, $t(\omega) \ge 0$: $F(\bar{u}(\omega)) = t(\omega)b$, $b^T \bar{u}(\omega) = \omega$.

- ω is a given parameter, t is additional unknown
- $\bullet \ \ \bar{u}(\omega) = \hat{u}(t(\omega)), \quad \omega \to +\infty \quad \Rightarrow \quad t(\omega) \to t_{\textit{lim}}, \ \|\bar{u}(\omega)\| \to \infty, \ \|\bar{u}(\omega)/\omega\| \to c < \infty$

Transformed problem and its optimization form: $v(\omega) = ar{u}(\omega)/\omega$

find
$$v(\omega) \in \mathbb{R}^n$$
, $t(\omega) \ge 0$: $F(\omega v(\omega)) = t(\omega)b$, $b^T v(\omega) = 1$.

$$\mathcal{I}_{\omega}(\mathbf{v}(\omega)) = \min_{\substack{\mathbf{v}\in\mathbb{R}^n\\b^{\top}\mathbf{v}=\mathbf{1}}} \mathcal{I}_{\omega}(\mathbf{v}), \qquad \mathcal{I}_{\omega}(\mathbf{v}) = \frac{1}{\omega}\mathcal{I}(\omega\mathbf{v}), \ \ \mathcal{I}'(\mathbf{v}) = F(\mathbf{v})$$

Limit analysis problem: $\omega \to +\infty$

$$t_{lim} = \inf_{\substack{oldsymbol{v} \in \mathbb{R}^n \ b^ op oldsymbol{v} = 1}} \mathcal{I}_\infty(oldsymbol{v}), \qquad \mathcal{I}_\infty = \lim_{\omega o +\infty} \mathcal{I}_\omega$$

• \mathcal{I}_{∞} is convex, 1-positively homogeneous, not finite-valued everywhere

• On a functional level, problem is defined on BD spaces, hidden constraint: $\operatorname{div} v = 0$

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Continuation strategy for determining t_{lim}



Generate (adaptively) a sequence 0 < ω₁ < ω₂ < ... < ω_N
 For any ω belonging to the sequence, find v(ω) ∈ ℝⁿ, t(ω) ≥ 0:

$$F(\omega v(\omega)) = t(\omega)b, \quad b^T v(\omega) = 1.$$

 $1 t_{lim} \approx t(\omega_N)$

Remarks:

- The increment of ω is increased if the increment of t is too small.
- The solver for fixed ω is initiated using solutions from previous 2 steps.

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Newton-like method for constraint optimization

The problem for given $\omega > 0$:

$$F_{\omega}(v^*) = t^*b, \ b^T v^* = 1 \quad \text{or} \quad \mathcal{I}_{\omega}(v^*) = \min_{\substack{v \in \mathbb{R}^n \\ b^T v = 1}} \mathcal{I}_{\omega}(v), \qquad F_{\omega}(v) = F(\omega v)$$

Semismooth Newton method as sequential quadratic programming:

$$\begin{aligned} u^{k+1} &:= u^k + s^k \qquad k = 0, 1, \dots, \quad u^0 - \text{ given}, \ b^\top u^0 = 1 \\ s^k &= \arg \min_{\substack{s \in \mathbb{R}^n \\ b^\top s = 0}} \left[\frac{1}{2} (F^o_\omega(u^k)s, s) + (F_\omega(u^k), s) \right] \\ \text{or } s^k &= h^k + \delta_k g^k, \quad F^o_\omega(u^k) g^k = b, \ F^o_\omega(u^k) h^k = -F_\omega(u^k), \ \delta_k = -\frac{b^\top h^k}{b^\top g^k} \end{aligned}$$

Crucial estimates implying local quadratic convergence:

$$\left(F_{\omega}^{o}(u^{k})(u^{k+1}-u^{*}), u^{k+1}-u^{*}\right) \leq \left(F_{\omega}(u^{k})-F_{\omega}(u^{*})-F_{\omega}^{o}(u^{k})(u^{k}-u^{*}), u^{*}-u^{k+1}\right)$$

• The algorithm can also be used for contact problems of E-P bodies.

We have also used damped and regularized versions of this algorithm.

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Solution corresponding to limit load factor t_{lim}



- solution for t_{lim} represents plastic collapse
- failure zone zone with discontinuity
- P1 elements lead to locking phenomena [Repin, S., Haslinger 2018]

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Mesh adaptive solution concept

- Apply the continuation over ω only on the coarsest mesh.
- Fix sufficiently large ω and use it for all finer meshed.
- Refine elements where higher strains appear.
- interpolate solution from the coarser mesh and use it for the initialization on a finer mesh.
- Use damped semismooth Newton method for finer meshes and the fixed ω_{\cdot}





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4. Brief notes to slope stability assessment.

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Limit vs. shear strength reduction analysis

Limit analysis:

- Factor of safety represents the limit load factor.
- Robust method supported by mathematical theory.
- Not so conventional in slope stability.

Shear strength reduction method:

- Conventional method in slope stability, implemented in many commercial codes.
- Strength parameters are reduced by a scalar factor up to the critical state. The safety factor represents the critical value.
- Iterative limit load methods can be applied [Tschuchnigg, Schweiger, Sloan 2015]
- Relationship between these two methods [S., Hrubešová, Michalec, Tschuchnigg 2021]

Basic elasto-plastic models used in geotechnics:

- Mohr-Coulomb or Drucker-Pragers yield criteria.
- They distinguish different behavior in tension and compression.
- Limit analysis for geotechnical models leads to conic optimization.



Application I – slope stability



- case study of a real slope in locality Doubrava (north-east part of Czechia)
- unstable slope with observed landslides, and various soil layers
- ullet numerical results confirmed that FoSpprox 1, mesh adaptivity was used
- [S., Hrubešová, Michalec, Tschuchnigg 2021]



Application II – river embankment



- case studies of a real river embankment in Lužec (near Prague)
- influence of pore pressure unconfined seepage problem, phreatic surface
- mesh adaptive solution for porous flow and mechanical problems
- [S., Tschuchnigg, Hrubešová, Michalec 2023]

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Application III – embankment dam



- benchmark problem with high embankment dam (more than 100 meters)
- sizes of the computational domain: 1200 x 500 meters
- one-sided coupling of porous flow and mechanical models
- [S., Tschuchnigg, Hrubešová, Michalec 2023]

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Conclusion

Summary:

- Selected Newton-like methods used in computational plasticity.
- Semismooth variants of the methods.
- Convergence analysis and numerical examples.
- Limit load and stability assessment.

Other related topics:

- Verification of the semismoothness for various E-P operators: [S. 2014], [S., Cermak, Kruis et al. 2016], [S., Cermak, Ligursky 2017]
- Development of in house codes in Matlab: [S., Cermak, Ligursky 2017], [Cermak, S., Valdman 2019], [Karátson, S., Béreš 2024]
- Duality and a posteriori error analysis for limit loads: [Repin, S., Haslinger 2018], [Haslinger, Repin, S. 2019], [S., Haslinger, Reddy, Repin 2021]
- Contact of E-P bodies and strain-gradient plasticity: [S., Haslinger, Hlaváček, Cermak 2015], [Reddy, S. 2020], [Reddy, S. 2024]





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Thank you for your attention!

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